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OHIO RIVER BASIN

SANDY CREEK, MERCER COUNTY

PENNSYLVANIA



# TAKE MITHETW DAW

NDI No. PA 00900 PennDER No. 43-53 SCS No. PA 475

# PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM



prepared for

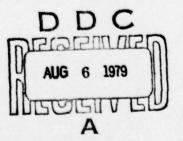
# **DEPARTMENT OF THE ARMY**

Baltimore District, Corps of Engineers
Baltimore, Maryland 21203

prepared by

# MICHAEL BAKER, JR., INC.

Consulting Engineers 4301 Dutch Ridge Road Beaver, Pennsylvania 15009



**July 1979** 

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#### OHIO RIVER BASIN

LAKE WILHELM DAM MERCER COUNTY, COMMONWEALTH OF PENNSYLVANIA NDI No. PA 00900 PennDER No. 43-53 SCS No. PA 475

(15) DACW31-79-C-0011

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National Dam Inspection Program. Wilhelm Dam (NDI Number PA-00900, PennDER Number 43-53, SCS Number PA-475) Ohio River Basin, Sandy Creek, Mercer County, Pennsylvania. Phase I Inspection Report,

410 795

# PREFACE

This report was prepared under guidance contained in the "Recommended Guidelines for Safety Inspection of Dams," for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I Investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I Inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established guidelines, the spillway design flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The spillway design flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

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#### PHASE I REPORT NATIONAL DAM INSPECTION PROGRAM

Lake Wilhelm Dam, Mercer County, Pennsylvania
NDI No. PA 00900, PennDER No. 43-53, SCS No. PA 475
Sandy Creek
Inspected 19 April 1979 and 4 June 1979

# ASSESSMENT OF GENERAL CONDITIONS

Lake Wilhelm Dam, approximately 41 feet high and 500 feet long, is a zoned earth embankment with a compacted fill cutoff trench. The dam is owned and operated by the Pennsylvania Department of Environmental Resources (PennDER), Bureau of State Parks. Lake Wilhelm Dam is categorized as a "High" hazard-"Large" size dam.

Hydraulic/hydrologic evaluations performed in accordance with procedures established by the Baltimore District, U.S. Army Corps of Engineers for Phase I Inspection Reports, revealed that the spillway will pass the Probable Maximum Flood (PMF) without overtopping the dam. Therefore, the spillway is assessed as "adequate".

The visual inspection and review of engineering data, made in April and May of 1979, revealed some problems that require remedial treatment but do not constitute any emergency conditions. The dam appeared to be in good overall condition at the time of the inspection. However, it is recommended that the owner:

- Initiate a monitoring program for the marshy areas to determine if quality or quantity changes take place and to institute appropriate action if required.
- 2) Develop a program whereby the movement of the riser could be monitored and appropriate remedial measures taken if required.
- 3) Repair eroded areas in the embankment by grading, treating and reseeding with an appropriate mixture to prevent erosion.
- 4) Install a permanent walkway or make necessary repairs on the downstream slope between the parking lot and crest of the dam.

- 5) Remove the vegetation growing within the riprapped areas.
- 6) Repair the concrete on the outlet head wall.

In addition, the following operational measures are recommended to be undertaken by the owner:

- Develop a detailed emergency operation and warning system.
- 2) During periods of unusually heavy rain, provide around-the-clock surveillance of the dam.
- 3) When warning of a storm of major proportions is given by the National Weather Service, the owner should activate the emergency operation and warning

CHUAN YUAN CHEN

EMGINEER
No. 14840 E

Submitted by:

MICHAEL BAKER, JR., INC.

C. Y. Chen, Ph.D., P.E.

Engineering Manager-Geotechnical

Date: 12 July 1979

Approved by:

DEPARTMENT OF THE ARMY

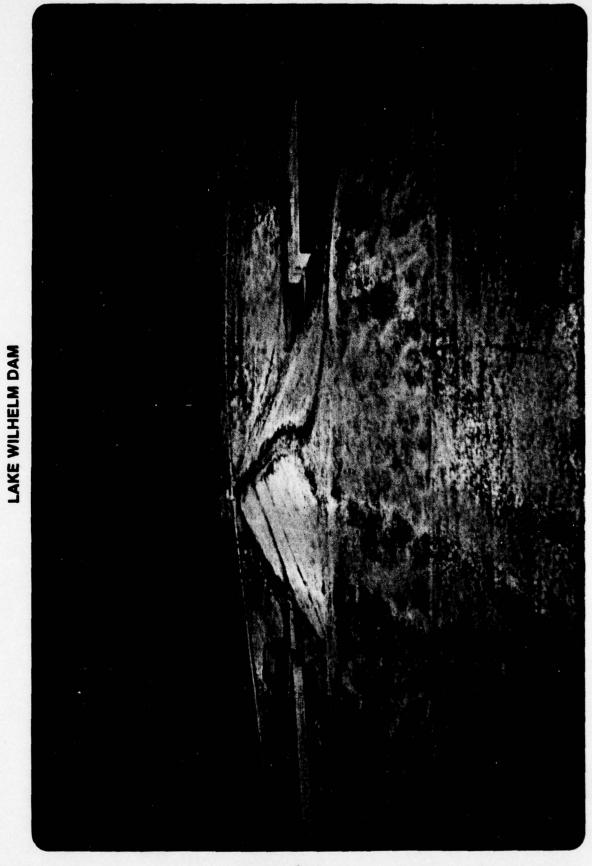
BALTIMORE DISTRICT, CORPS OF ENGINEERS

AMES W. PECK

Colonel, Corps of Engineers

District Engineer

Date: 21 July 1919



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# PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM LAKE WILHELM DAM NDI No. PA 00900, PennDER No. 43-53, SCS No. PA 475

SECTION 1 - PROJECT INFORMATION

# 1.1 GENERAL

- a. Authority The Dam Inspection Act, Public Law 92-367, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a program of inspection of dams throughout the United States.
- b. Purpose of Inspection The purpose of the inspection is to determine if the dam constitutes a hazard to human life or property.

# 1.2 DESCRIPTION OF PROJECT

Description of Dam and Appurtenances - Lake Wilhelm Dam, also known by its U.S. Department of Agriculture, Soil Conservation Service (SCS) number PA 475, was built for flood control and recreation. The dam, which was designed by the SCS, is a zoned earth embankment with a crest length of approximately 500 feet and a maximum height of 41.5 feet. The upstream face has a slope of 3H:1V (Horizontal to Vertical) to El. 1191.5 feet and a 2.5H:1V slope to the top of dam El. 1211.5 feet. To increase structural stability, two 4-foot berms are located at El. 1191.5 feet and 1194.5 feet, a 20-foot berm is at El. 1180.0 feet. The downstream face has a slope of 2.5H:1V and the crest width is 16 feet.

A 4-foot wide foundation drain trench containing granular material was installed to a maximum depth of about 8 feet beneath the downstream toe of the dam. Sections of this trench in the valley bottom contain 12-inch diameter perforated corrugated metal collector pipes which discharge from the sides of the reinforced concrete outlet structure at the downstream toe of the dam. Toe drains of granular material and rockfill were installed along portions of the contacts of the downstream slope with both abutments.

The outlet works (principal spillway in SCS terminology) consists of a reinforced concrete two stage riser inlet structure connected to two 6-foot-square concrete conduits which are approximately 150 feet long. The low stage overflow is at El. 1192.2 feet with the high stage weir constructed at El. 1194.7 feet. The outlets of the riser structure, located beneath the embankment, are contained in a reinforced concrete box culvert fitted with seven anti-seep collars. downstream end of the outlet pipe discharges into a reinforced concrete impact basin, the design of which is based on the Saint Anthony Falls (SAF) research. Chute blocks, baffle blocks and an end sill are provided. The length of the basin is 54 feet and the width between training walls is 22 feet. The reinforced concrete riser unit is a large drop-inlet type spillway. The concrete box has four openings on each side. Each opening has a weir length of 15 feet. The pond drain consists of two 66-inch-square manually operated sluice gates.

The emergency spillway is located along the left abutment. The channel is a vegetated earth type with an overall length of 500 feet and a bottom width of 80 feet. The right side of the channel has a side slope of 3H:1V and the left side slope measures 2.5H:1V. The entrance section of the earth spillway rises from the reservoir at a 0.1 percent slope to the crest of the 100-foot long control section (El. 1199.0 feet). From the control section to the downstream channel, the profile of the emergency spillway declines at a slope of 2.0 percent.

- b. Location Lake Wilhelm Dam is located on Sandy Creek approximately 6 miles northwest of its confluence with French Creek in Sandy Lake Township, Mercer County, Pennsylvania. The dam is located 0.6 mile from the intersection of PA Route 173 and PA L.R. 43068, and approximately 1.0 mile from the center of Sandy Lake, Pennsylvania. The dam can be located on USGS Quadrangle, Sandy Lake, Pennsylvania, with coordinates N 41° 22' 12" W 80° 05' 12". The location of Lake Wilhelm Dam is shown on Plate 1.
- C. <u>Size Classification</u> The maximum height of the dam is 41.5 feet and the reservoir volume to dam crest is 66,400 acre-feet. The dam is therefore in the "Large" size category.

- d. Hazard Classification Due to the proximity of several homes immediately downstream and the town of Sandy Lake, Pennsylvania located approximately 1.0 mile from the dam, many lives could be lost in the event of a dam failure. Therefore, the dam is classified in the "High" hazard category.
- e. Ownership The dam is owned by the Mercer County Commissioners, Mercer County Courthouse, Mercer, Pennsylvania 16137.
- f. Purpose of Dam Lake Wilhelm Dam is used for floodwater detention and also for recreation in conjunction with the Maurice K. Goddard State Park.
- Design and Construction History Lake Wilhelm Dam was designed by the SCS under the authority of the Watershed Protection and Flood Prevention Act, Public Law 566, as amended. The dam was constructed by Brodhead Construction Company of Aliquippa, Pennsylvania from August 1967 through October 1969. Two work stoppages occurred during the construction; one was caused by severe weather in the Winter of 1967 and the other was a scheduled six-month shutdown. A portion of the embankment (approximately 10,000 C.Y. or one-sixth of the total) was placed between the dates of 11 August 1967 and 1 September 1968. At this time the work was suspended for 6 months or until the fill settlement had reached the required level. The following year on 26 May 1969 the contractor resumed operations and after removing the first few feet of fill continued to build up the embankment and impermeable core until its completion in October 1969.
- h. Normal Operational Procedures The lake is normally maintained at the low-level inlet of the riser structure, El. 1192.20 feet. There has reportedly been no major flood since the dam was constructed. The maximum height of the pool as marked on the riser structure is at El. 1193.50 feet. The dam is inspected on a yearly basis according to procedures for SCS dams. Routine maintenance is performed by the state park personnel.

# 1.3 PERTINENT DATA

a.	Drainage Area (square miles) -	56.5
b.	Discharge at Dam Site (c.f.s.) -	
	Maximum Known High Water at Dam Site (El. 1193.5 ft., June 1972) - Outlet Works at Maximum Pool (El. 1211.5 ft.) - Spillway Capacity at Maximum Pool (El. 1211.5 ft.) -	680 2365 8635
c.	Elevation (feet above Mean Sea Level [	M.S.L.]) -
	Design Top of Dam - Actual Top of Dam -	1211.5 Varies from 1211.8 to 1212.2
	Maximum Design Pool - Riser Crest - Emergency Spillway Crest - Normal Pool - Streambed at Centerline of Dam - Maximum Tailwater -	1211.5 1192.2 1199.0 1192.2 1170+ Not available
d.	Reservoir (miles) -	
	Length of Maximum Pool - Length of Normal Pool -	13.74 9.47
e.	Storage (acre-feet) -	
	Top of Dam (El. 1211.5 ft.) - Spillway Crest (El. 1199.0 ft.) - Normal Pool (El. 1192.0 ft.) -	66,400 31,250 17,825
f.	Reservoir Surface (acres) -	
	Top of Dam (El. 1211.5 ft.) - Spillway Crest (El. 1199.0 ft.) - Normal Pool (El. 1192.0 ft.) -	3510 2250 1680
g.	Dam -	
	Type - Zoned earth embankment containing 61,347 c.y. of fill  Length (feet) -  Maximum Height (feet) -  Crest Width (feet) -  Side Slopes - Upstream -  to El. 1191.5 ft  El. 1191.5 ft.  to crest -	500 41.5 16 3H:1V 2.5H:1V
	Downstream -	2.5H:1V

- Zoning The center impervious zone consists of silty clayey sand (SC) provided with a cutoff trench. The upstream and downstream shell sections consist of gravelly (GP-GW) materials.
- Cutoff Compacted earth with maximum base width of 20 feet in foundation and lower abutments
- Drains Foundation drain trench with granular material and 12-inch diameter perforated corrugated metal collector pipes in valley bottom; toe drains of granular material and rockfill along portions of downstream slope junctions with both abutments.
- h. Diversion and Regulating Tunnel None
- i. Spillway (Emergency Spillway in SCS Terminology) -

Type - Vegetated earth channel in left abutment
Length (feet along centerline) - 500
Base Width (feet) - 80
Side Slopes - Right Side 3H:1V
Left Side 2.5H:1V
Crest Elevation (feet M.S.L.) - 1199.0
Gates - None
Downstream Channel - Spillway exits into natural
stream channel approximately
20 feet wide

- j. Regulating Outlets Two 66-inch-square, flange frame type control gates. The rising stem is constructed of 1.25-inch diameter stainless steel with a fully adjustable stem guide fitted with bronze bushings. The hand-operated crank is connected to the pedestal base lift with a bronze lift nut.
- k. Principal Spillway -
  - Type Two-stage inlet riser and two 6-foot-square concrete conduits

First Stage Orifice Crest Elevation (feet M.S.L.) - 1192.2
Width (feet) - 8 each at 15.0
Vertical Clearance (feet) - 5.00
Second Stage Orifice -

Crest Elevation (feet M.S.L.) - 1194.7
Width (feet) - 8 each at 15.0
Vertical Clearance (feet) - 2.50

Outlet Pipe - Consists of two 6-foot-square concrete conduits approximately 150 feet long. The outlets are contained in a reinforced concrete box culvert fitted with seven anti-seep collars.

Riser Floor Invert Elevation
(feet M.S.L.) - 1169.2
Outlet Conduit Exit Invert Elevation
(feet M.S.L.) - 1162.8

#### SECTION 2 - ENGINEERING DATA

# 2.1 DESIGN

Lake Wilhelm Dam was designed by the SCS. Design data included in this report were obtained from:

- 1) SCS Drawings No. PA-475-P, "Sandy Creek Watershed, Multiple Purpose Dam PA-475, Crawford and Mercer Counties, Pennsylvania," 48 sheets, designed 1966, "as built" 1969. (Copies of sheets 4, 5, 6, 9, 18, 19, 21 and 48 are included in this report as Plates 3-10; prints of other sheets are available in Pennsylvania Department of Environmental Resources' [PennDER] and SCS's files.)
- 2) Dam Permit Application Report prepared by the Pennsylvania Department of Forests and Waters (predecessor of PennDER) on 3 June 1966.
- "Design Report, Site PA-475, Sandy Creek, Pennsylvania," by the SCS.
- 4) "Sandy Creek Watershed Work Plan," report prepared by Mercer County Commissioners, et al., April 1962.

# 2.2 CONSTRUCTION

Chronological information concerning the construction of Lake Wilhelm Dam was presented in paragraph 1.2.g. The information was obtained from the files of PennDER and the Mercer County Conservation District office. During construction of the dam, the SCS provided full-time inspection. The semi-monthly inspection reports of the construction progress are available in PennDER's files. A representative of the Pennsylvania Department of Forests and Waters (now PennDER) made periodic visits to the dam during construction. Memoranda, and black and white photographs of construction progress are also available in PennDER's files.

# 2.3 OPERATION

Lake Wilhelm is operated at normal pool throughout the year. The maintenance personnel visit the dam daily in order to read the staff gage located on the intake riser assembly. Records of these readings are on file in the park office.

# 2.4 EVALUATION

- a. Availability The information reviewed consisted of PennDER's file on the dam and information obtained from the owner's representative.
- b. Adequacy The information available is adequate for a Phase I Inspection.
- c. Validity There is no indication at the present time to doubt the validity of the available engineering data.

#### SECTION 3 - VISUAL INSPECTION

# 3.1 FINDINGS

- a. General The dam and its appurtenant structures were found to be in good overall condition at the time of the inspection, with the exception of two wet areas in the emergency spillway channel. Noteworthy deficiencies observed are described briefly in the following paragraphs. The complete visual inspection check list and field sketch are given in Appendix A.
- b. Dam A bare, eroded pedestrian path is present on the downstream face of the dam leading from the parking lot and sanitary station to the crest of the dam. Several smaller ruts and erosion paths were noted on the embankment (see field sketch for locations).

The riprap on the upstream face and around the outlet basin is overgrown with vegetation in several areas.

A marshy area exists in the approach channel of the emergency spillway. The wet zone is on the left side of the channel near the control section. The area at the end of the discharge channel is also wet and marshy.

- c. Appurtenant Structures The concrete in the intake riser assembly and outlet structure appeared to be in good condition. The cursory survey made at the time of the visual inspection indicates the riser structure has undergone a differential movement of approximately 2.5 inches. Erosion was noted around the outlet head wall and wing walls. On 4 June 1979 during a site visit, a horizontal crack was observed immediately above the outlet conduits.
- d. Reservoir Area The reservoir slopes are moderately sloping and consist primarily of farmland and second growth forests.
- e. Downstream Channel The slopes adjacent to the downstream channel are relatively steep and partially wooded. The slope of the downstream channel is mild, averaging approximately 12 feet per mile. The Borough of Sandy Lake is located about 1 mile downstream from the dam. Approximately 40 homes are located in the floodplain area below the dam at the north end of the Borough of Sandy Lake.

### SECTION 4 - OPERATIONAL PROCEDURES

# 4.1 PROCEDURES

There are no formal emergency procedures in the event of an impending catastrophe involving the dam. It is understood that the condition of the dam is checked by Maurice K. Goddard State Park personnel daily in conjunction with the reading of the staff gage located on the intake riser assembly. The spillway and outlet works are uncontrolled. Two 66-inch-square manually operated sluice gates are available for drawdown.

It is recommended that formal emergency procedures be prepared, prominently displayed and furnished to all operating personnel.

# 4.2 MAINTENANCE OF DAM

Although routine upkeep is presently performed by the state park personnel, maintenance of the dam is the responsibility of the Mercer County Commissioners. No records of the routine maintenance are kept.

# 4.3 MAINTENANCE OF OPERATING FACILITIES

The operating equipment is inspected, operated and lubricated twice a year by the state park maintenance personnel.

# 4.4 DESCRIPTION OF ANY WARNING SYSTEM IN EFFECT

There is no warning system or procedure in the event of a dam failure. An emergency warning procedure should be developed.

# SECTION 5 - HYDRAULIC/HYDROLOGIC

# 5.1 EVALUATION OF FEATURES

a. Design Data - Hydrologic and hydraulic design calculations for Lake Wilhelm Dam were obtained from the SCS "Design Report." The dam was designed to reduce floodwater damages and is accordingly capable of providing protection for a 100-year frequency storm. The elevations of the design high water and top of dam were determined by routing the emergency spillway and freeboard hydrographs through the reservoir. Both hydrographs were based on a storm duration of 6 hours. A brief summary of the rainfall and hydrograph data used in the analysis is as follows:

Hydrograph	6-hour Rainfall (inches)	Runoff (inches)	Hydrograph Peak (c.f.s.)		
Emergency Spillway	7.81	5.23	25,060		
Freeboard	21.25	18.21	108,415		

The results of the flood routing analysis are as follows:

Hydrograph	Peak Inflow (c.f.s.)	Maximum Outflow (c.f.s.)	Maximum Reservoir Elevation (feet M.S.L.)
Emergency Spillway Freeboard	25,060 108,415	3,030 11,000	1199.8 1211.5

- b. Experience Data The greatest flood of record, since construction of the reservoir, occurred in June 1972. According to the "Post Flood Report for Tropical Storm Agnes" the Lake Wilhelm watershed received an average of 4 inches of rainfall during the period of 20-25 June 1972.
- c. <u>Visual Observations</u> No condition was observed at the time of the inspection to indicate that the spillway and outlet works could not operate satisfactorily in the event of a flood.

- d. Overtopping Potential Lake Wilhelm Dam is classified as a "High" hazard-"Large" size dam requiring evaluation for a spillway design flood equal to the Probable Maximum Flood (PMF). Since the dam was designed by the SCS using a spillway design flood developed with the Probable Maximum Precipitation (PMP) [Refer to page 2 of 6, Appendix D], no further hydrologic or hydraulic analysis was performed.
- e. Spillway Adequacy The dam, as outlined above, was designed based on a freeboard hydrograph which is essentially equal to the PMF. Therefore, the spillway is "adequate" according to the recommended criteria.

### SECTION 6 - STRUCTURAL STABILITY

# 6.1 EVALUATION OF STRUCTURAL STABILITY

- a. Visual Observations No structural inadequacies were noted during the visual inspection of the dam. The wet and marshy areas indicated in paragraph 3.1.b. are not considered detrimental to the stability of the dam according to the conditions present at the time of inspection. The differential movement of the riser intake assembly does not appear to have an effect on the structural stability at the present time. It is recommended, however, that a monitoring program be established and appropriate remedial actions be taken, if necessary.
- b. Design and Construction Data The dam was designed and constructed according to standard SCS procedures for structures of this type. According to the SCS "Design Report," the upstream slepe of the dam has a safety factor of approximately 2.0 under rapid drawdown conditions and the downstream slope has a safety factor of approximately 1.7 under steady seepage conditions.
- c. Operating Records Nothing in the readily available operating information would lend itself to questioning the relative structural stability of the embankment.
- d. <u>Post-Construction Changes</u> There have been no post-construction changes which would adversely affect the structural stability of the dam.
- e. Seismic Stability The dam is located in Seismic Zone I of the "Seismic Zone Map of the Contiguous United States, "Figure 1, page D-30, "Recommended Guidelines for Safety Inspection of Dams." This is a zone of very low seismic activity. Experience indicates that dams in Seismic Zone I will have adequate stability under seismic loading conditions if they have adequate stability under static loading conditions. Therefore, if the monitoring program indicates that the movement of the intake riser (with remedial measures, if necessary) does not effect the static stability of the dam, then further consideration of seismic stability is not necessary.

# 7.1 DAM ASSESSMENT

- a. Safety The dam and its appurtenant structures were found to be in good overall condition at the time of inspection. Lake Wilhelm Dam is evaluated as being a "High" hazard-"Large" size dam in accordance with the "Recommended Guidelines for Safety Inspection of Dams" and should have a spillway capacity equal to the PMF. As presented in Section 5, the spillway and reservoir were determined to be of sufficient size to pass PMF. Based on this investigation, the spillway capacity is assessed as "adequate."
- b. Adequacy of Information The information available and the observations made during the field inspection are considered sufficient for this Phase I Inspection Report.
- c. <u>Urgency</u> The owner should initiate without delay the recommendations discussed in paragraph 7.1.d.
- d. Necessity for Additional Data/Evaluation The visual inspection indicated the existence of two marshy areas in the emergency spillway channel. The area in the approach channel is believed to be the result of natural springs; however, the cause of the marshy area in the exit channel could not be determined. It is therefore recommended that a monitoring program for the marshy areas be established to determine if quantity or quality changes take place and to institute appropriate action, if necessary.

Review of a survey and inspection report dated 23 November 1976 indicated that a slight uplift of the riser had occurred along with some settlement of the principal spillway. During our visual inspection on 19 April 1979, a cursory survey of the embankment and appurtenances was made and our findings also indicated some differential movement of the riser structure. According to the personnel at the Mercer County SCS office, as part of their annual late fall inspection routine, the water in the lake is lowered and the inside of the outlet conduit is examined. The movement of the riser could cause a break in the outlet conduit and thereby create an uncontrolled discharge from the

dam. It is therefore recommended that the owner initiate a program whereby the movement of the riser could be monitored more closely in order to avert any major problems.

# 7.2 RECOMMENDATIONS/REMEDIAL MEASURES

The inspection and review of information revealed certain items of work which should be performed without delay by the owner. These include:

- The owner should initiate a monitoring program for the marshy areas to determine if quantity or quality changes take place and to institute appropriate action, if necessary. If the cause of both areas is the result of natural springs, the installation of spring drains is recommended.
- The owner should initiate a program whereby the movement of the riser could be monitored and appropriate remedial measures taken, if required.

In order to correct operational, maintenance and repair deficiencies, the following measures are recommended to be undertaken by the owner in a timely manner:

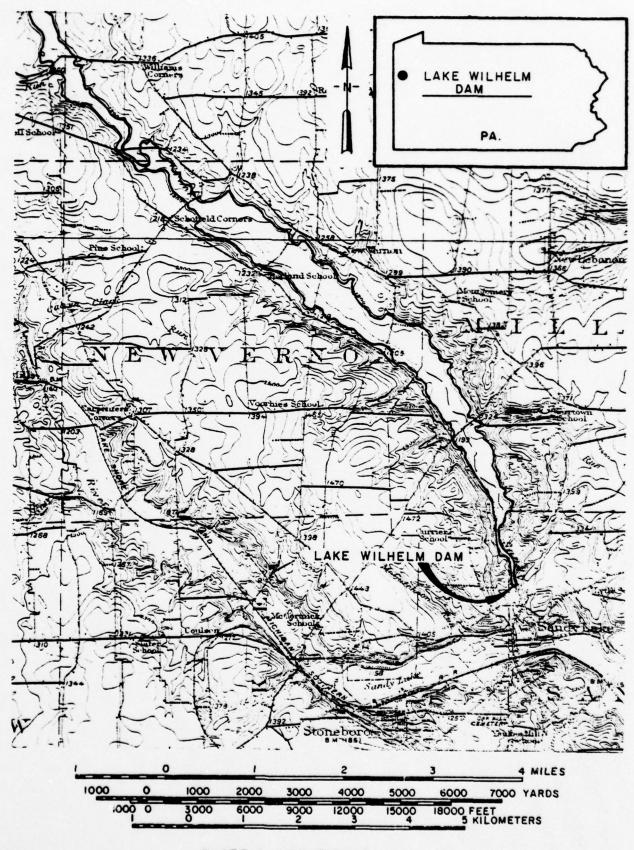
- The eroded areas should be graded, treated and seeded with an appropriate seeding mixture to prevent erosion.
- 2) A permanent walkway should be installed or necessary repairs made on the downstream face leading from the parking lot to the crest of the dam. A permanent walkway would eliminate the damage to the embankment caused by the heavy pedestrian traffic in this area.
- 3) The overgrowth of vegetation should be removed from the riprap.
- 4) The crack in the head wall above the outlet conduits should be repaired.

The owner should continue in the future to inspect the embankment and concrete appurtenances, and repair as necessary.

In addition, the following operational measures are recommended to be undertaken by the owner:

- Develop a detailed emergency operation and warning system.
- 2) During periods of unusually heavy rain provide around-the-clock surveillance of the dam.
- When warning of a storm of major proportions is given by the National Weather Service, the owner should activate the emergency operation and warning system.

PLATES



LAKE WILHELM DAM

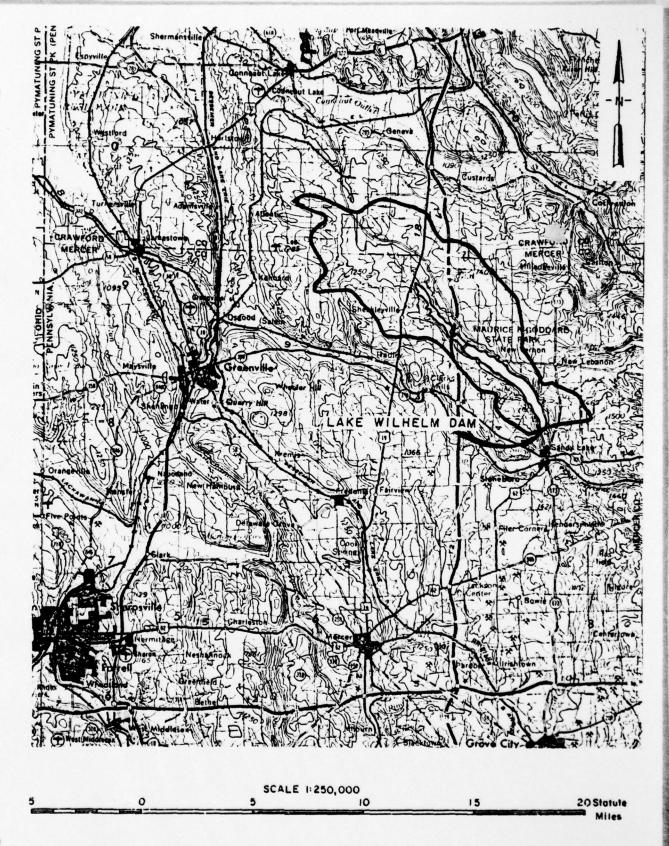
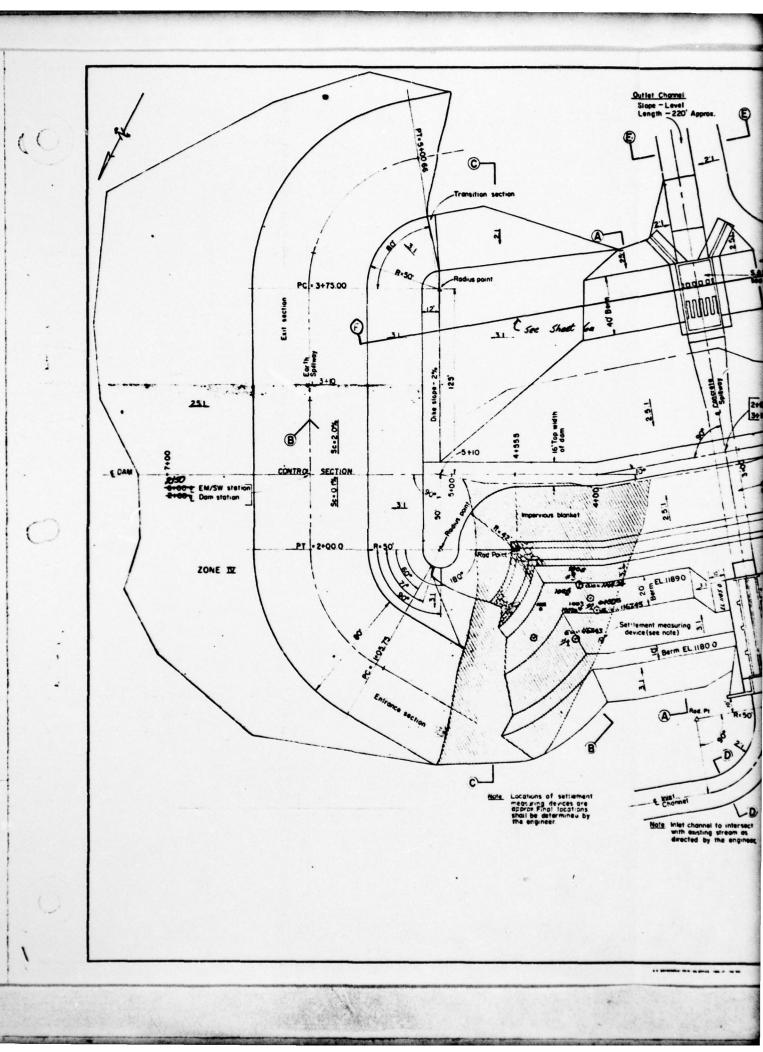
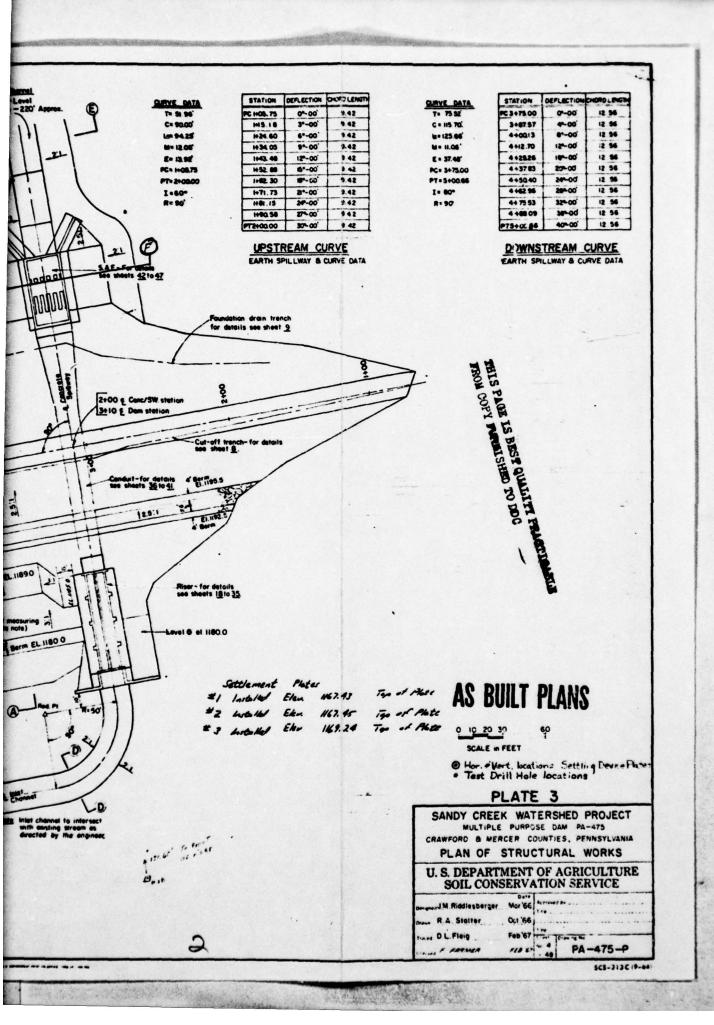
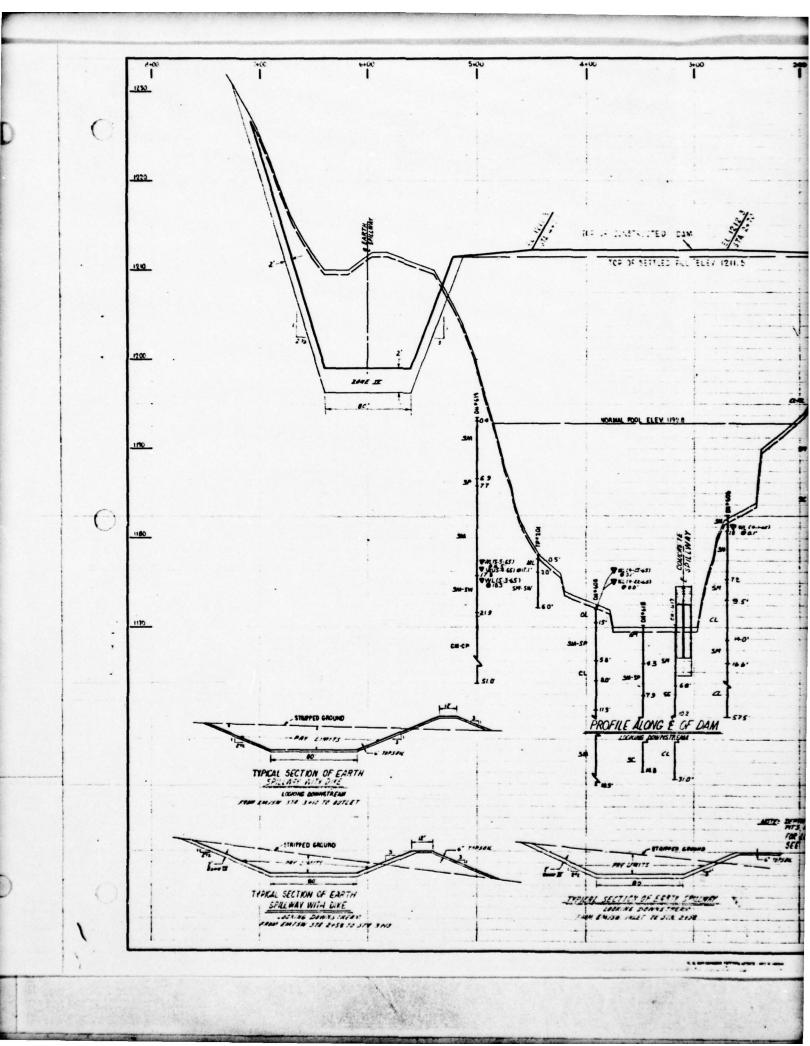
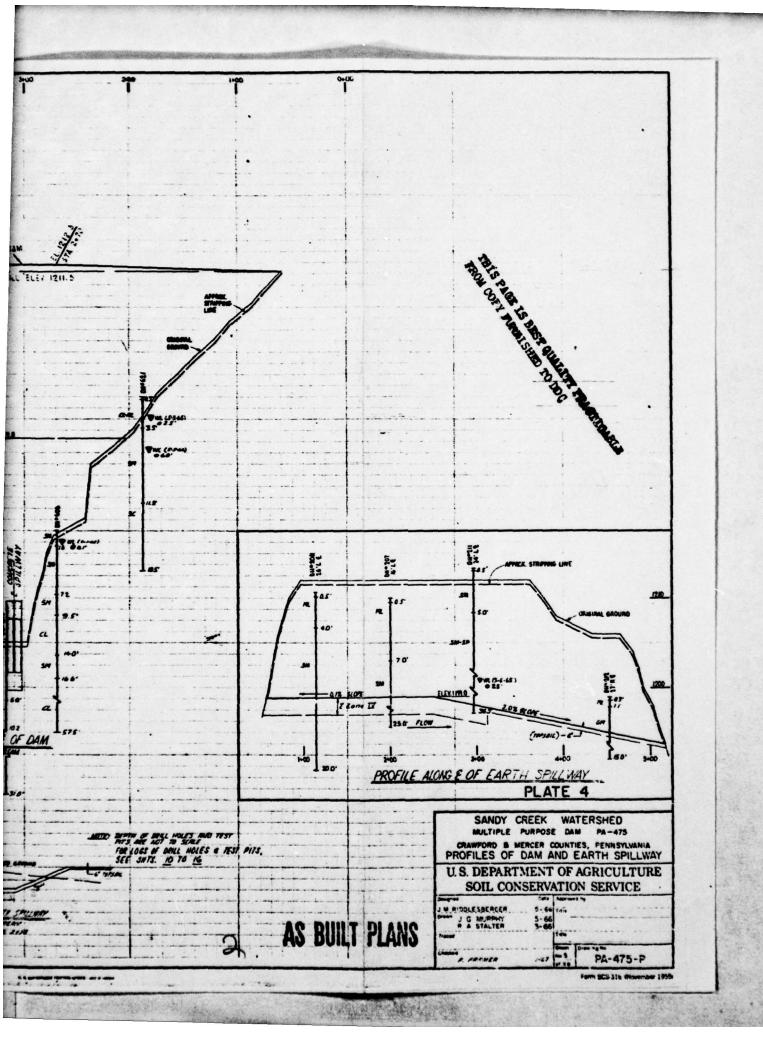


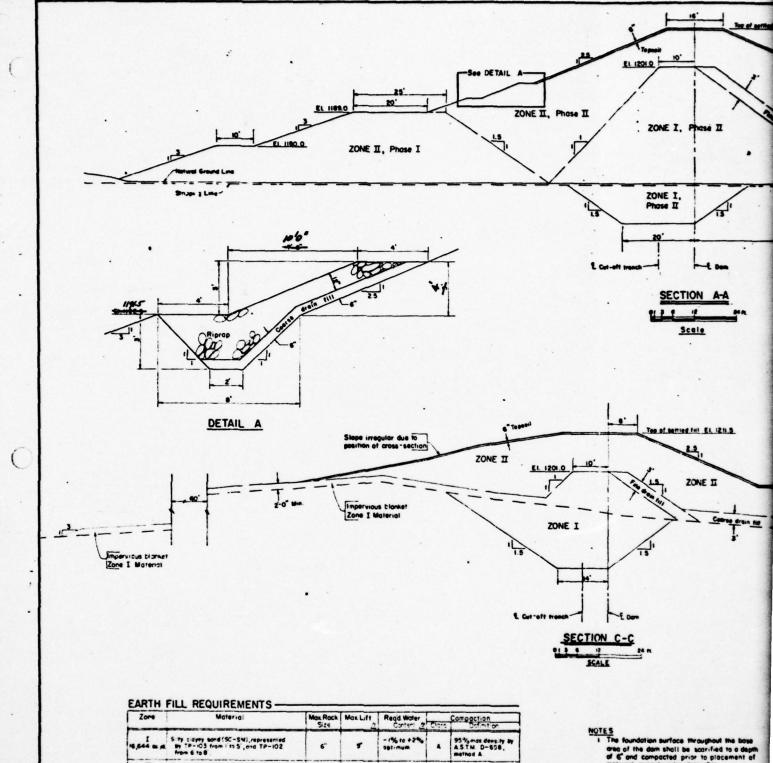
PLATE 2 WATERSHED MAP











Zore	Material	Max Rock Size	Max Lift	Regid Water	Compaction		
-				Content 2	Chin	Definition	
16,644 m gt	5-ty clayer sand (SC-SM), represented by TP-103 from 1 to 5", and TP-102 from 6 to 8".	6"	•	-1% to +2%	4	95% max dens ty by A S T M D-658, method A	
4,419 cs yd	Gravel (SP-GM), represented by TP-202 from 1.5' to 11.0', TP-102 from 0.6' to 6.0', TP-104 from 4.5' to 8.5'.	6"	•	optimum to +3%	٨	95% max density by A.S.T.W. D-698, method C.	
ш	Gueralized rock roked from other zones	10"	16	Any	×	See specifications	
M	Siffy clayey sand (SC-SM) , represented by TP-103 from (155)	6	•	-1% to +2%	3	See specifications	

Mas Lift Michness prior to compoction

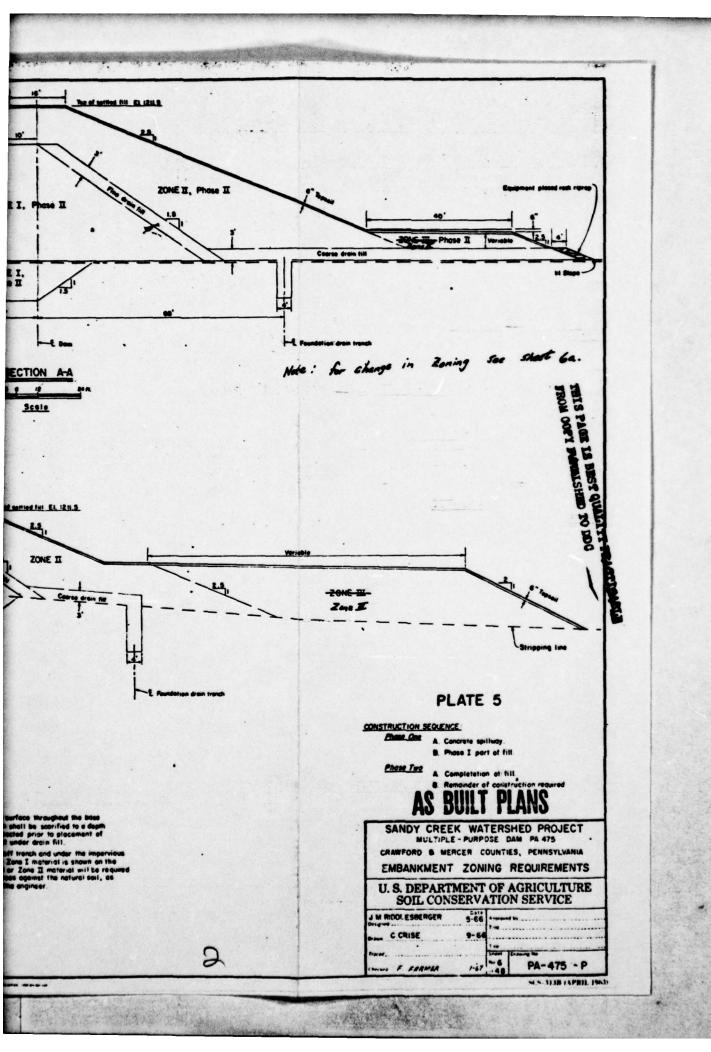
Safer content at time of placement.

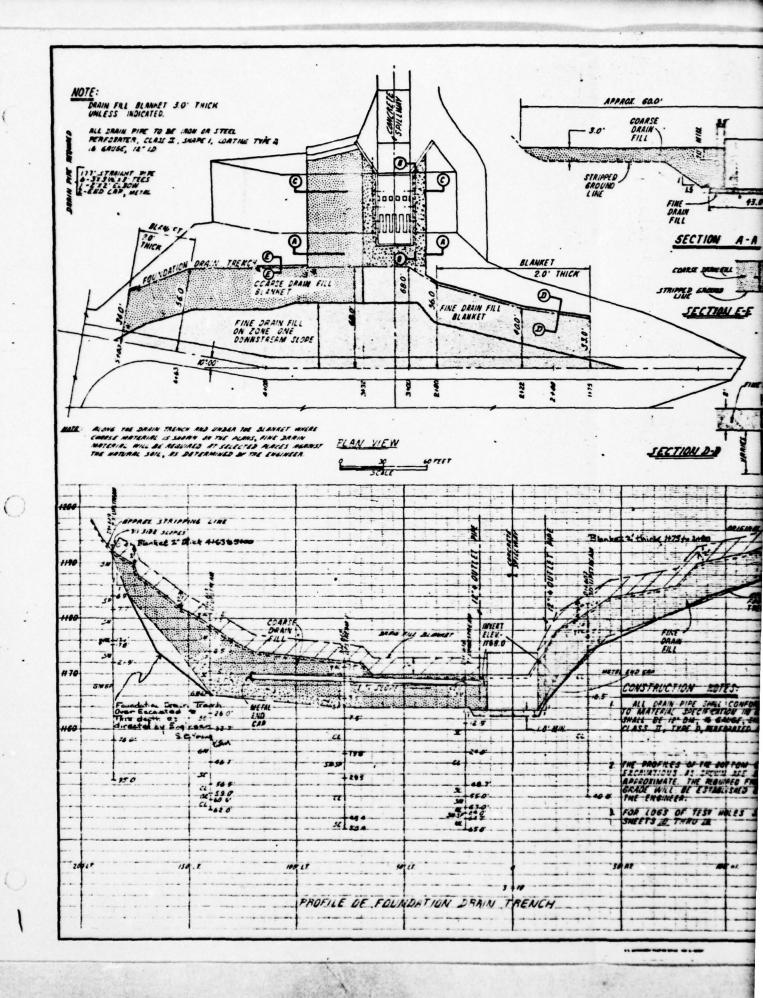
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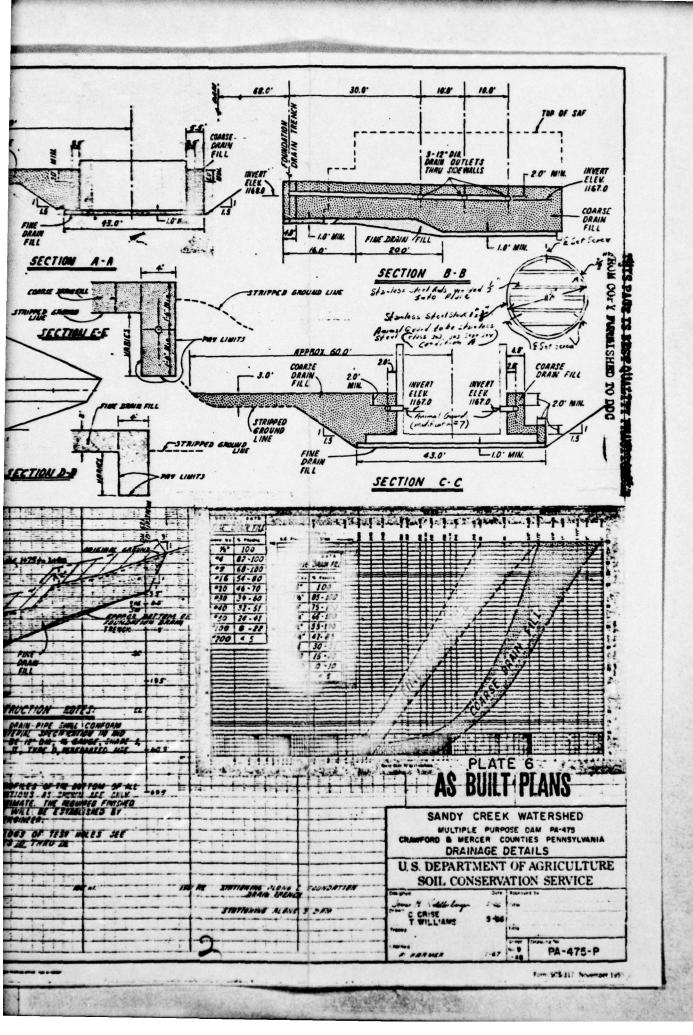
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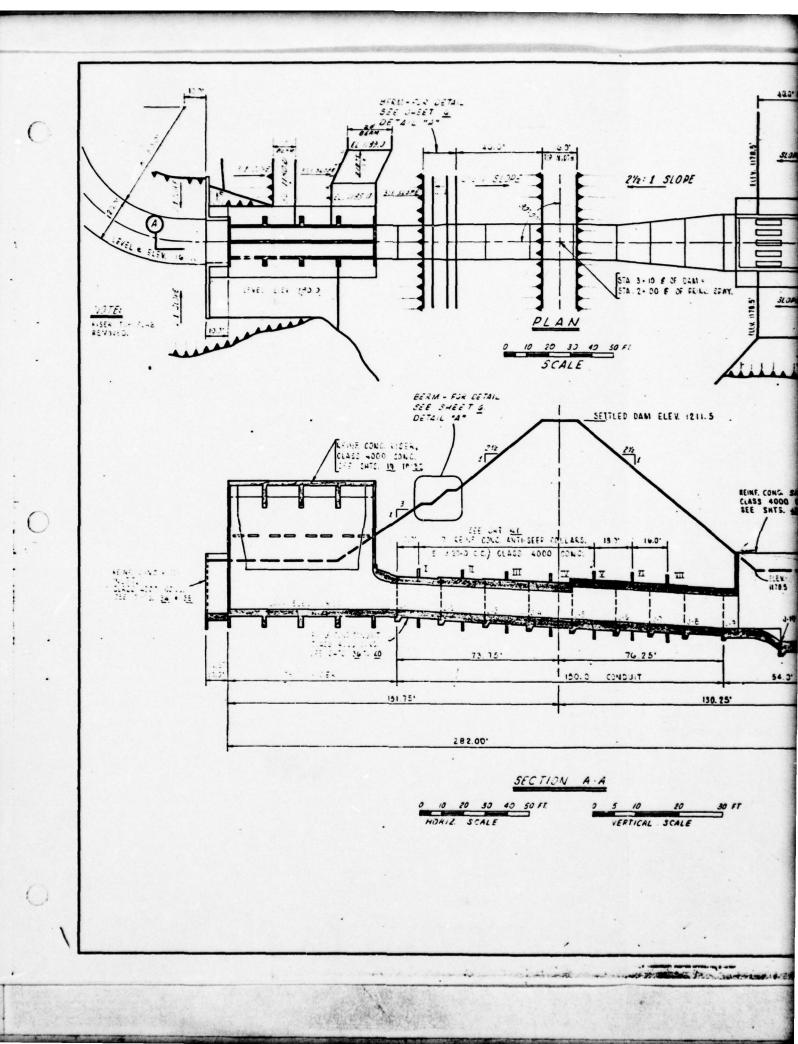
- The foundation surface throughout the base are of the dam shall be scarified to a day of 6" and compacted prior to placement a material, except under drain fill.
- Along the cut-off trench and under the imperal blonket, where Zone I material is shown on the plans, drain full or Zone II material will be re-et selected places against the natural soil, de-determined by the engineer.

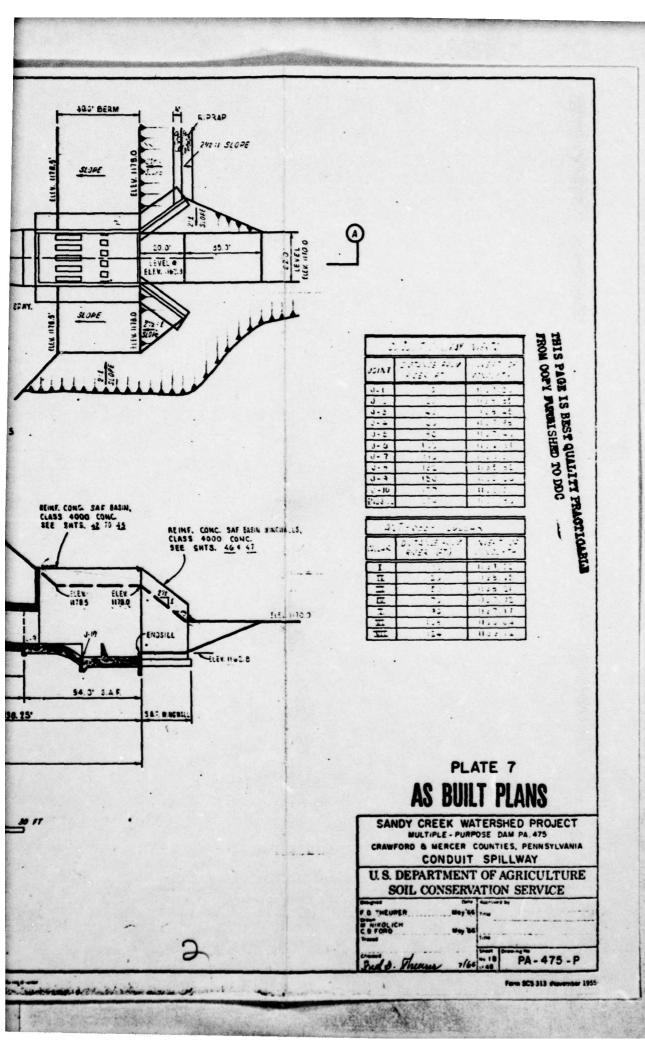
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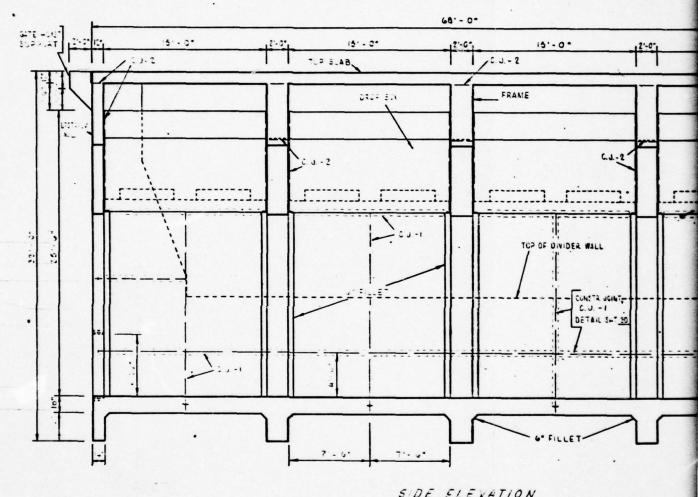




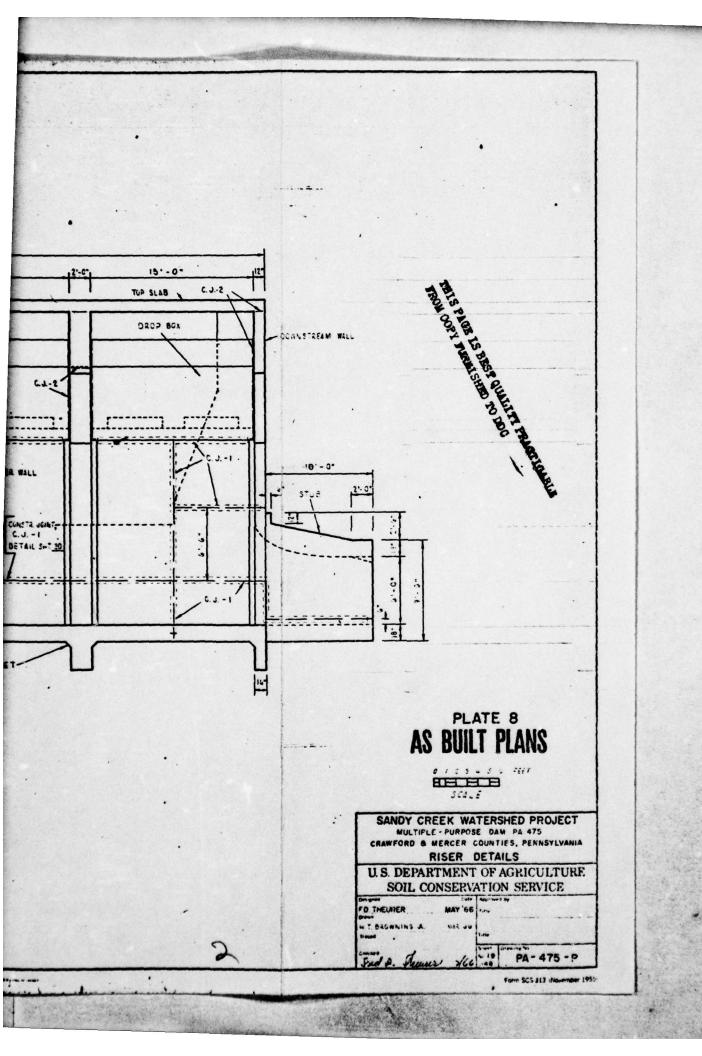


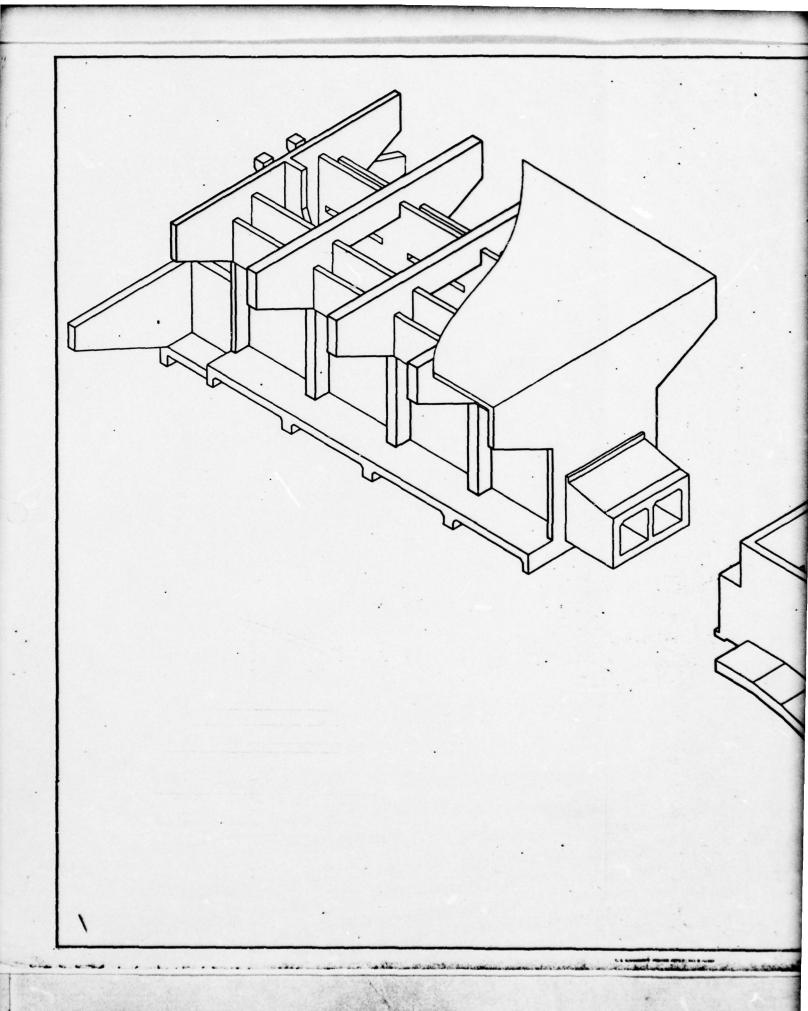


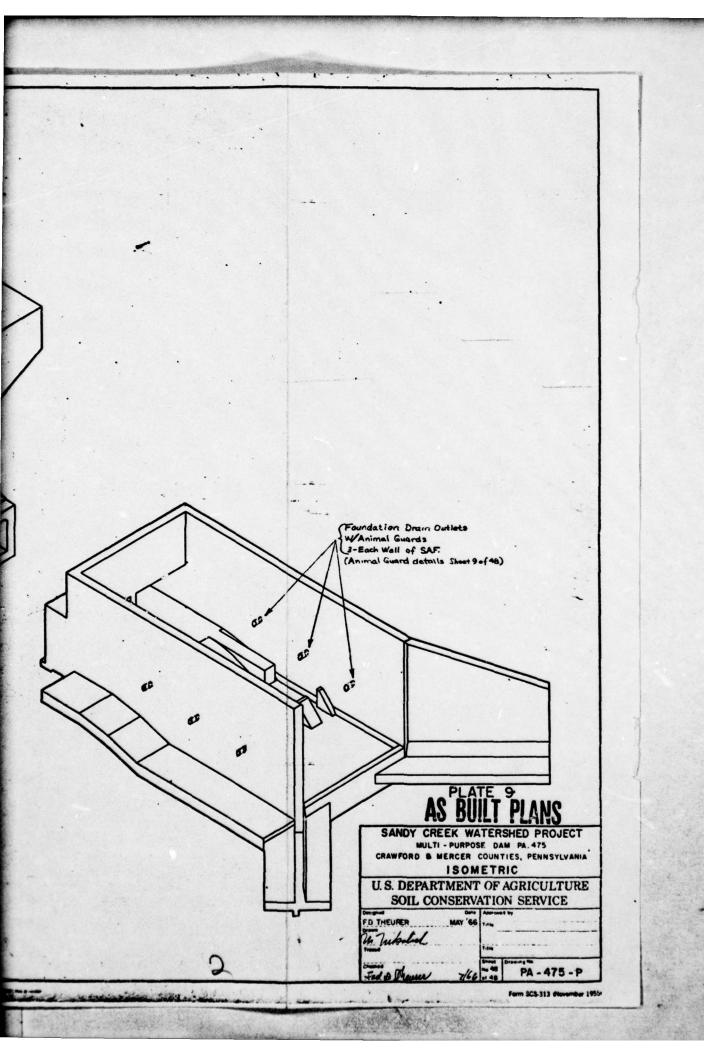


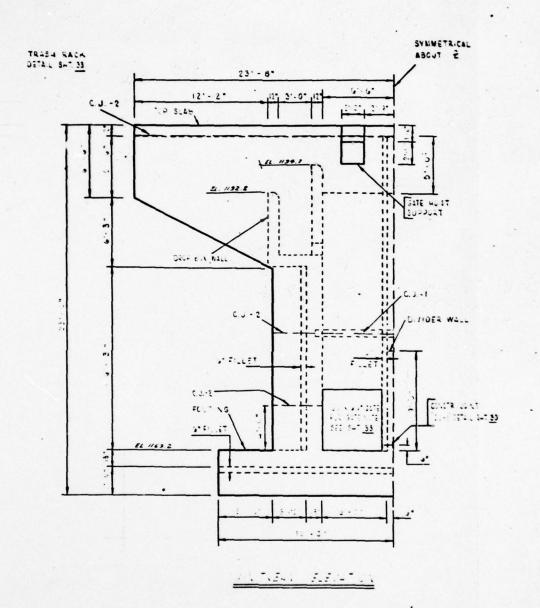


SIDE ELEVATION





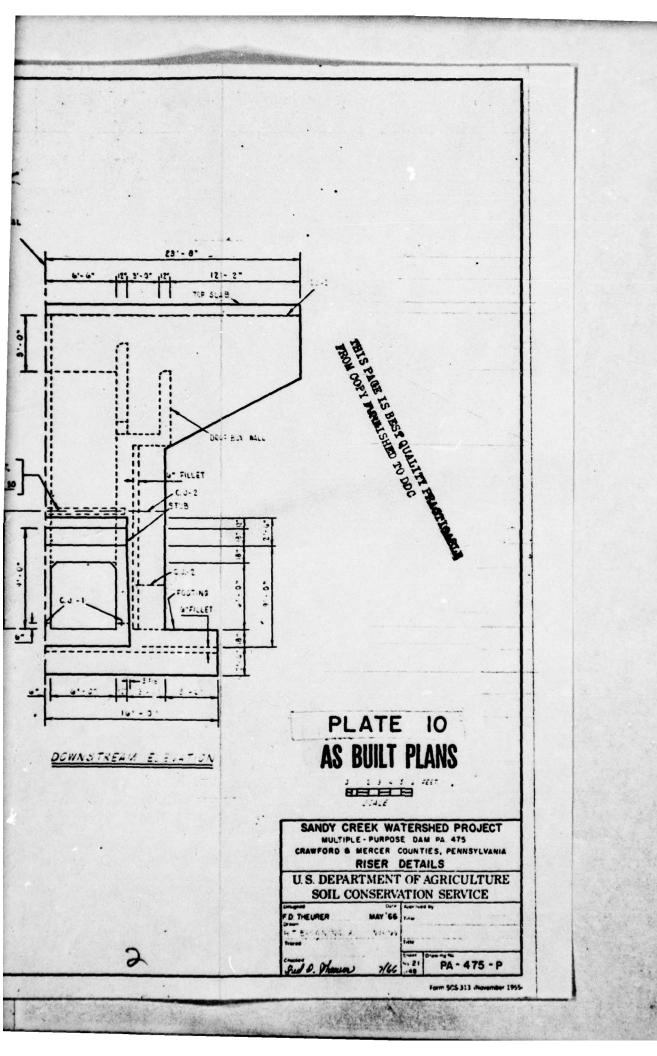




SYMMETRICAL

ABOUT &

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### APPENDIX A

CHECK LIST - VISUAL INSPECTION AND FIELD SKETCH

### Check List Visual Inspection Phase 1

Coordinates Lat. N 41° 22.2' Long. W 80° 05.2'	Temperature 50°F.	Time of Inspection 1172.20 ft. M.S.L.*	top of the concrete head wall of the outlet structure to information contained in "as built" plans from SCS.	Owner's Representatives:
PA	Temper	lwater at	wall of the wall o	
Btate	Weather Sunny, Windy	.M.S.L. Tai	oncrete head n contained i	
nty <u>Mercer</u>	Weather	1192.80 ft	of the conformation	Jr., In
Name of Dam Lake Wilhelm Dam County NDI # PA 00900 PennDER # 43-53 SCS # PA 475	Date of Inspection 19 April 1979	Pool Blevation at Time of Inspection 1192.80 ft. M.S.L.* Tailwater at Time of Inspection 1172.20 ft. M.S.L.*	*Elevations are based on the top 81.80 ft. M.S.L. according to in	Inspection Personnel: Michael Baker, Jr., Inc.:

Ward Guelich - Maint. Repair I

Recorder

David Johns

Site Visit on 4 June 1979

Dr. C. Y. Chen James G. Ulinski

Rodney E. Holderbaum James G. Ulinski David Johns A-2

CONCRETE/MASONRY DAMS - Not Applicable

REMARKS OR RECOMMENDATIONS OBSERVATIONS Name of Dam: LAKE WILHELM DAM
NDI # PA 00900 VERTICAL AND HORIZONTAL ALIGNMENT VISUAL EXAMINATION OF STRUCTURAL CRACKING CONSTRUCTION JOINTS SURPACE CRACKS
CONCRETE SURPACES MONOLITH JOINTS

A-3

CONCRETE/MASONRY DAMS - Not Applicable

## **EMBANKMENT**

Name of Dam: LAKE WILHELM DAM
NDI # PA 00900

ISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SURPACE CRACKS	No surface cracks were observed.	The embankment is well vegetated with grasses and crown vetch.

UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOE

No unusual movement was observed.

 A bare, eroded pedestrian path is present on the downstream face leading from the parking lot and sanitary station to the crest of the dam.

SLOUGHING OR EROSION OF EMBANKMENT AND ABUTMENT

. Recommend installation of permanent walkway to prevent further reoccurance.

Several ruts and small erosion paths were noted on the crest and upstream face.

2

2. The ruts and erosion paths should be regraded, treated and seeded with an appropriate mixture to prevent erosion.

3. Erosion was observed around the stilling basin. 3. Reco

asin. 3. Recommend that the area be regraded, treated and seeded to prevent erosion. If the problem reoccurs, then riprap should be placed.

VERTICAL AND HORIZONTAL No misalignment was noted.

The riprap on the upstream face and around the outlet basin is overgrown with vegetation in several areas.

RIPRAP PAILURES

n Recommend removal of the overgrowth from riprapped areas.

Embankment drains were installed; however, due to the height of the tailwater, no assessment could be made.

DRAINS

## OUTLET WORKS

NDI # PA 00900  VIBUAL EXAMINATION OF CONCRETE SURFACES IN OUTLET CONDUIT  INTAKE STRUCTURE However was low crack v		OF OBSERVATIONS  ING OF The concrete appeared to be in very good condition.  The riser inlet structure is in good condition. The only problem noted was the differential movement of approximately 2.5 inches.  The outlet structure is in good condition; no problems were noted.  However, during a site visit on 4 June 1979, the tailwater was lower than during the visual inspection and a horizontal crack was observed above the outlet conduits.	A monitoring program should be established and remedial measures taken if required.  The crack on the head wall should be be repaired.
OUTLET CHANNEL	The outlet chan side for approvere were noted.	The outlet channel is protected with riprap on the right side for approximately 50 ft. downstream. No problems were noted.	
EMBRGENCY GATE	Two 66-insquar inlet structure.	Two 66-insquare sluice gates were installed in the riser inlet structure. These gates were inaccessible.	These gates are partially opened periodically.

Name of Dam: LAKE WILHELM DAM

UNGATED SPILLWAY (Emergency Spillway)

OBSERVATIONS

REMARKS OR RECOMMENDATIONS

CONTROL SECTION

VIBUAL EXAMINATION OF

NDI # PA 00900

The emergency spillway is a vegetated earth side channel. No erosion or other problems were observed at the control section.

APPROACH CHANNEL

The approach channel is well vegetated with grasses and crown vetch. A wet area was observed on the left side of the channel near the control section.

DISCHARGE CHANNEL

The well vegetated discharge channel exits into Sandy Creek a short distance below the dam. The area at the end of the discharge channel was wet and marshy at the time of aspection.

BRIDGE AND PIERS

None

Name of Dam: LAKE WILHELM DAM NDI # PA 00900	GATED SPILLMAY - Not Applicable	<b>у-8</b>
VISUAL EXAMINATION OF	OBSERVATIONS REMARKS OR	REMARKS OR RECOMMENDATIONS
CONCRETE SILL		
APPROACH CHANNEL		
DISCHARGE CHANNEL		
BRIDGE AND PIERS		
GATES AND OPERATION EQUIPMENT		

OTHER

### RESERVOIR

Name of Dam: LAKE WILHELM DAM
NDI # PA 00900

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SLOPES	The reservoir slopes are moderately sloping and consist primarily of farmland and forests.	The reservoir slopes are stable from soil mechanics and hydraulics (erosion) standboints.

The reservoir was designed by the SCS with allowance for 100 years of sediment accumulation. No sedimentation problems were noted. SEDIMENTATION

REMARKS OR RECOMMENDATIONS

# DOWNSTREAM CHANNEL

Name of Dam: LAKE WILHELM DAM
NDI # PA 00900

OBSERVATIONS VISUAL EXAMINATION OF

(OBSTRUCTIONS, DEBRIS, ETC.) CONDITION

The downstream channel is free of debris and other obstructions. A few small bridges are located downstream, but do not appear to present any problems.

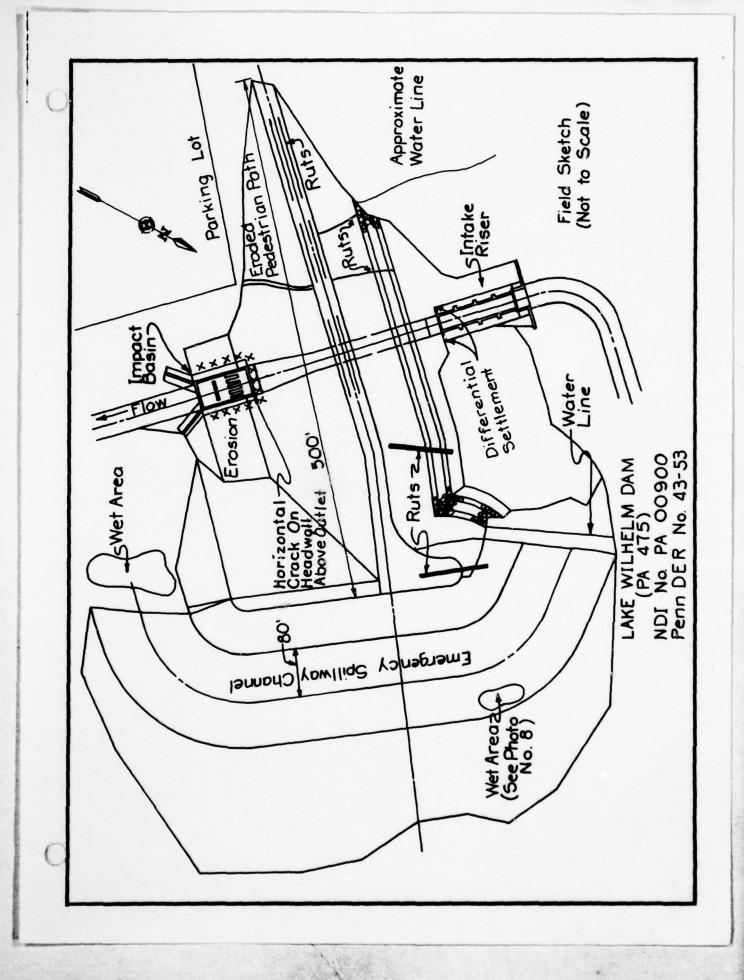
SLOPES

relatively steep and partially wooded. The slope of the downstream channel is mild, averaging approximately 12 ft. per mi. The slopes adjacent to the downstream channel are

> APPROXIMATE NO. OF HOMES AND

POPULATION

The Borough of Sandy Lake is located approximately i mi. downstream from the dam. The population of Sandy Lake (1970 Census) was 772 persons. An estimated 40 homes are located on the north side of Sandy Lake in the immediate floodplain below the dam.



### APPENDIX B

CHECK LIST - ENGINEERING DATA

# ERGINEERING DATA DESIGN, CONSTRUCTION, OPERATION

Name of Dam: LAKE WILHELM DAM NDI # PA 00900

ITEH

REMARKS

See Plate 3 - Plan of Dam. PLAN OF DAM See Plate 1, a portion of a USGS 15 minute Stoneboro, PA quadrangle map showing the dam location with state location inset. REGIONAL VICINITY MAP

Construction of the dam started on 21 August 1967 and finished on 31 October 1969. The work was done by Brodhead Construction Co. The construction was shut down upon occasion for bad weather and also for 6 months to allow the embankment to consolidate. CONSTRUCTION HISTORY

See Plates 4 and 5. TYPICAL SECTIONS OF DAM Design computations are included in the SCS "Design Report" and summarized in Appendix D of this report. HYDROLOGIC/HYDRAULIC DATA

OUTLETS - PLAN See Plate 7.

- DETAILS

See Plates 8 and 10. CONSTRAINTS DISCHARGE RATINGS are included in the SCS "Design Report" and Appendix D of this report.

None available RAINFALL/RESERVOIR RECORDS

Name of Dam: LAKE WILHELM DAM
NDI # PA 00900

IN THE PARTY OF TH

DESIGN REPORTS

The SCS report, "Sandy Creek, Site PA - 475," was available through PennDER.

GEOLOGY REPORTS See A

See Appendix E, also "Design Report" from SCS - available through PennDER.

Seepage and Design computations were done by the SCS for hydrology and hydraulics. stability studies were also done by the SCS. HYDROLOGY & HYDRAULICS DESIGN COMPUTATIONS SEEPAGE STUDIES DAM STABILITY

A foundation and borrow investigation was performed with test pits and test borings; the computations are contained in the SCS "Design Report." Boring records are contained as Sheets 3 and 11-17 of the design drawings. MATERIALS INVESTIGATIONS BORING RECORDS LABORATORY FIELD

Due to the slight movement of the riser intake structure, a survey was done on 16 November 1976 by SCS engineers. The results are contained in the PennDER file No. 43-53. POST-CONSTRUCTION SURVEYS OF DAM

The majority of the borrow material necessary for the embankment was available from the emergency spillway excavation. These materials are largely the silty sands and gravels used for the shell material and for the impermeable core. BORROW SOURCES

Name of Dam: LAKE WILHELM DAM
NDI # PA 00900

ITEM REMARKS

A staff gage is located on the riser intake structure. MONITORING SYSTEMS

# MODIFICATIONS None

The daily staff A high water mark is located on the riser intake structure, El. 1193.70 ft. gage readings are taken and the log is available at the park office. HIGH POOL RECORDS

POST-CONSTRUCTION ENGINEERING Annual STUDIES AND REPORTS the Mei

Annual inspections have been made from 1971 to 1976 by representatives of the Mercer County SCS office and the State Park Superintendent's office. Copies of these inspections are available in the PennDER files.

PRIOR ACCIDENTS OR FAILURE OF DAM None DESCRIPTION REPORTS

The log is available Park personnel visit the riser inlet structure daily to read the staff gage. The log is available at the Maurice Goddard State Park office. Records of routine maintenance are not kept by the park personnel. MAINTENANCE OPERATION RECORDS

Name of Dam: LAKE WILHELM DAM
NDI # PA 00900

SPILLMAY PLAN See Plate 3.

ITEN

REMARKS

SECTIONS See Plate 4.

DETAILS See Plates 8 and 10.

The 66-in.-square manually operated sluice gates are located in the riser intake structure; no detailed drawings are available; photographs of sluice gates installed are available in PennDER file No. 43-53. OPERATING EQUIPMENT PLANS & DETAILS

### CHECK LIST HYDROLOGIC AND HYDRAULIC DATA ENGINEERING DATA

DRAINAGE AREA CHARACTERISTICS: 56.5 sq.mi. (predominately wooded)
ELEVATION TOP NORMAL POOL (STORAGE CAPACITY): 1192.2 ft. (17,700 acft.)
1199.0 ft.
ELEVATION TOP FLOOD CONTROL POOL (STORAGE CAPACITY): (31,250 acft.)
ELEVATION MAXIMUM DESIGN POOL: 1199.80 ft. (Design High Water)
ELEVATION TOP DAM: 1212.0 ft. (minimum elevation). 1212.2 ft. (average elevation
CREST: Emergency Spillway
a. Elevation 1199.0 ft.
b. Type Vegetated side channel
c. Width 80 ft.
d. Length Approximately 500 ft.
e. Location Spillover Left abutment area of dam
f. Number and Type of Gates None
OUTLET WORKS:Conduit Spillway
a. Type Twin 6-ftsquare reinforced concrete conduits
b. Location Approximately 210 ft. from left end of embankment
c. Entrance inverts El. 1107 2 ft
d. Exit inverts E1. 1162.80 ft.
e. Emergency draindown facilities Two 66-insquare sluice gates
HYDROMETEOROLOGICAL GAGES:Not Applicable
a. Type
b. Location
c. Records
MAXIMUM NON-DAMAGING DISCHARGE Unknown

APPENDIX C

**PHOTOGRAPHS** 

### DETAILED PHOTOGRAPH DESCRIPTIONS

- Overall View of Dam View from Left Abutment; Emergency Spillway in Foreground, Intake Riser to Right and Outlet Channel to Left
- Photo 1 Intake Riser Assembly
  (Orange marks above existing pool indicate previous highest water level.)
- Photo 2 Intake Riser Assembly as seen from Emergency Spillway (View shows high stage inlets)
- Photo 3 St. Anthony Falls (SAF) Type Outlet Structure (The majority of cover on the embankment is crown vetch which remains dormant until late spring. The crown vetch therefore is brown in the photos and the eroded areas that were reseeded with grasses have already turned green, thereby accenting the eroded areas in the pictures.)
- Photo 4 Outlet Structure and Downstream Area
  (Note vegetation growing through riprap and reseeded area in embankment.)
- Photo 5 Downstream Channel as seen from Emergency Spillway Exit
- Photo 6 Entrance to Emergency Spillway Channel as Viewed from Atop Left Abutment (Wet area is near center of photo.)
- Photo 7 Eroded Pedestrian Path on Downstream Face
  Leading from Parking Lot to Crest of Dam
  (Green grass on both sides of path indicates that
  attempts were made to control erosion. Recommend
  permanent steps be installed in this area.)
- Photo 8 Marshy Area Located in Entrance Channel of Emergency Spillway

Note: Photographs were taken on 19 April 1979.



PHOTO 1. Intake Riser Assembly
(Orange Marks Above Existing Pool Indicate Previous Highest Water Level)



PHOTO 2. Intake Riser Assembly as Seen from Emergency Spillway (View Shows High Stage Inlets)



PHOTO 3. St. Anthony Falls (SAF) Outlet Structure (The majority of cover on the embankment is crown vetch which remains dormant until later in the spring. The crown vetch therefore is brown in the photos and the eroded areas that were reseeded with grass have already turned green, thereby accenting the eroded areas in the photos.)

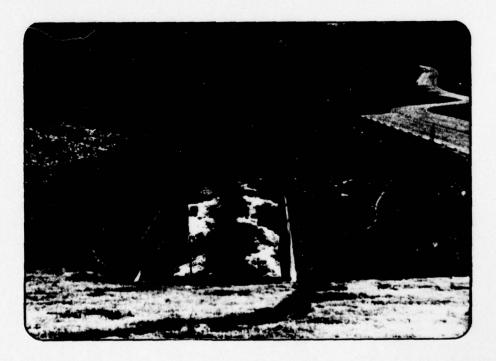


PHOTO 4. Outlet Structure and Downstream Area (Note Vegetation Growing Through Riprap and Reseeded Area in Embankment)



PHOTO 5. Downstream Channel as seen from Emergency Spillway Exit



PHOTO 6. Entrance to Emergency Spillway Channel as Viewed from atop Left Abutment (Wet Area is near Center of Photo)



PHOTO 7. Eroded Pedestrian Path on Downstream Face Leading from Parking Lot to Crest of Dam (Green grass on both sides of path indicates that attempts were made to control erosion. Recommend permanent steps be installed in this area.)



PHOTO 8. Marshy Area Located in Entrance Channel at Emergency Spillway

### APPENDIX D

HYDROLOGIC AND HYDRAULIC COMPUTATIONS

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	Stage Vs. Stor		<u> </u>
	Stage VS. Dis		4
	Top of Dam	Profile	5
	-Map of down	nstream	6
	damage al	rea	· · · · · · · · · · · · · · · · · · ·

MICHAEL BAKER, JR., INC.

THE BAKER ENGINEERS

Box 280 Beaver, Pa. 15009

Subject Lake Wilhelm Dam	S.O. No
	Sheet No of
	Drawing No
DELL	

Lake Wilhelm Dam was designed by the SCS in accordance with standard criteria circa 1966. The design flood was based on rainfall essentially equal to the probable maximum precipitation. Therefore, the dam should be capable of passing the probable maximum flood (PMF) without overtopping. In view of the above no additional hydrologic or hydraulic calculations were performed for this report. The SCS calculations were reviewed, however, and summarized in this appendix.

In addition, the conclusions presented pertain to present conditions, and the effect of future development on the hydrology has not been considered.

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		Point	Areal	(in)	Peak flow	
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	Emergency	9.2	7.81		25,060	
	Energency spilluray	9.2	7.81	5.23	25,060	
	Energency spilluray	9.2	7.81	5.23	25,060	
	Emergency spillway Freeboard	9.2	7.81	5,23  8.21	75,060 	
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MICHAEL BAKER, JR., INC.

THE BAKER ENGINEERS

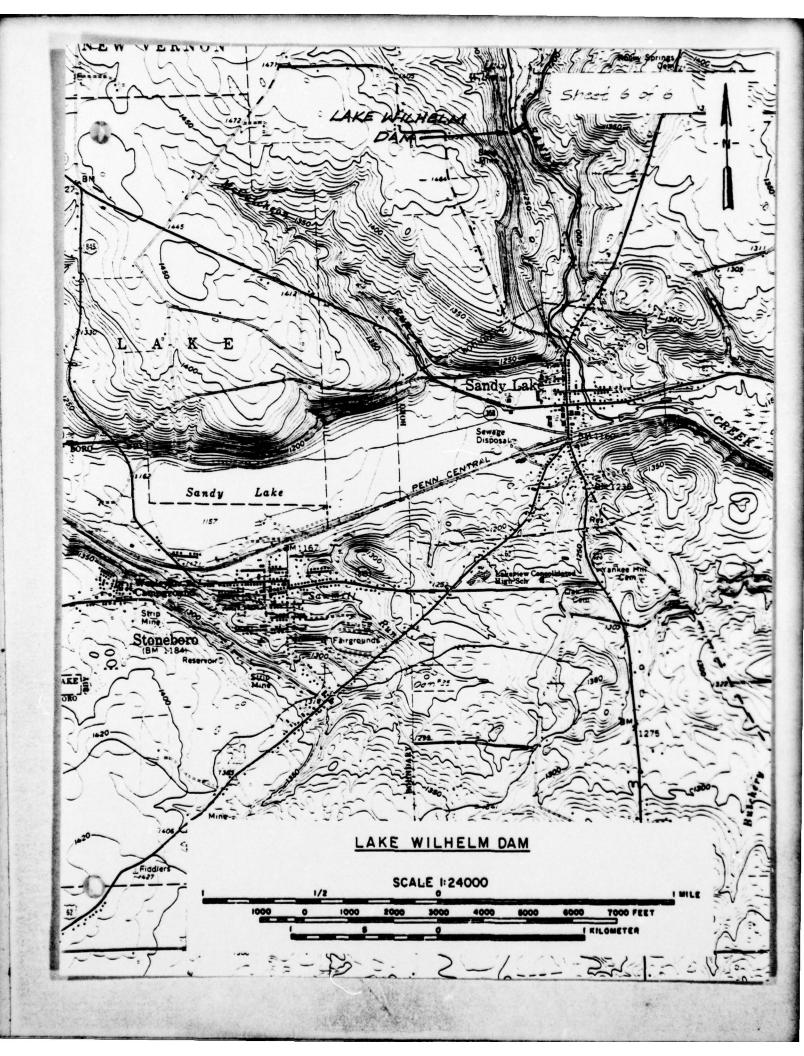
Box 280 Beaver, Pa. 15009 

	Disc	charge	
Elev. (ft.)	Outlet Norts (cfs.)	Spillmay (cfs)	Remarks
11920			Normal pool
1192.5	152		
1193.0	372		
11935	- 683		
1194.0	993		
1/94.5	1066		High stage inlet crest
1195.0	1231		Inlet crest
11955	1505		
11960	1618		
-1196.5	1722		
1197.0	1828		
11975	1950		
1198.0	_ 1961		
1199.0	1982	0	Spillway Crest
12005	2032		
1205.0	2175		
1211.5	2365	8635	Top of Dam

The above information was taken from the scs Design Report for Wilhelm Dam.

Information concerning the origin of this data is also contained in the design report.

Subject LAKE WILHELM DAM MICHAEL BAKER, JR., INC. S.O. No.\_\_\_\_ THE BAKER ENGINEERS TOP OF DAM PROFILE Sheet No. 5 of 6 Drawing No. \_\_ Box 280 Dote 5-9.79 Computed by \_\_\_SCB Checked by REH Beaver, Pa. 15009 ELEVATION (feet)



APPENDIX E

REGIONAL GEOLOGY

### LAKE WILHELM DAM NDI No. PA 00900, PennDER No. 43-53, SCS No. PA 475

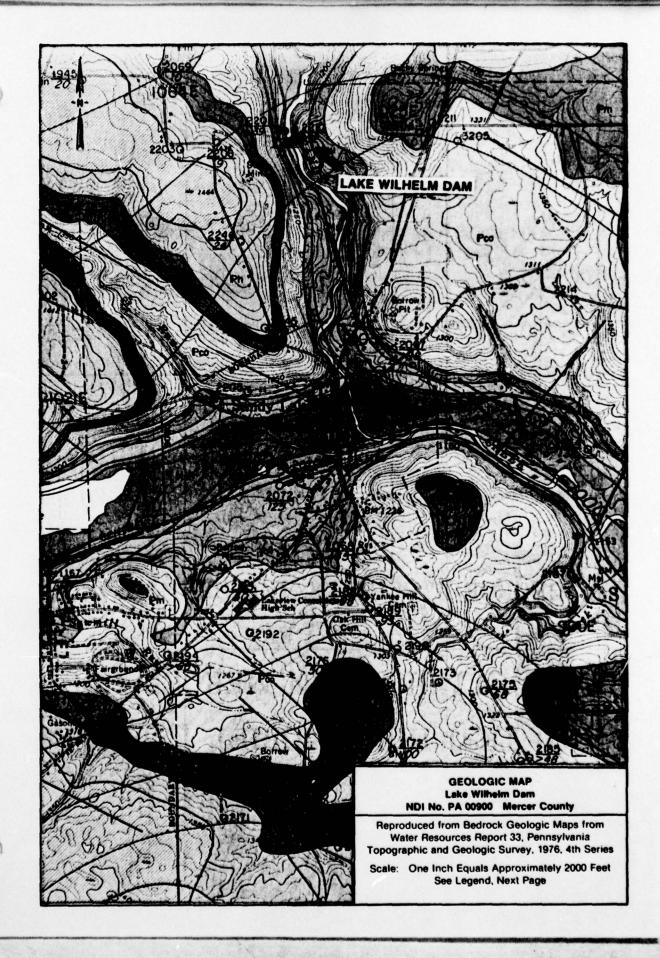
### REGIONAL GEOLOGY

Lake Wilhelm Dam was constructed across the valley of Sandy Creek, an area of thick glacial deposits which, in places, exceeds 60 feet in depth. A geologic report prepared by the SCS for design of the dam, describes in detail the complex glacial history of the site. As the result of several glacial advances and retreats, combined with erosion and impoundment of meltwater in the valley, the soils at the dam site are a complex series of discontinuous beds of sands, gravels, and varved lacustrine silts and clays separated by erosional surfaces. Some peat deposits were also formed during deposition of recent alluvium.

Bedrock units underlying the glacial till in this section of the Appalachian Plateaus physiographic province are interbedded shale and sandstone members of the Shenango formation, Mississippian system. An outcrop of sandstone was reported above the area of the right abutment.

In several of the borings, artesian flow occurred from the zone of weathered bedrock and some seepage was observed below the sandstone outcrop.

The dam site is shown in relationship to the regional geology on the map on the following page.



### **LEGEND**

PENNSYLVANIAN

Pottsville Group

### MERCER FORMATION

Mostly dark-gray shale, but contains thin beds of coal and limestone and lenses of sandstone. Generally unimportant as an aquifer, but locally yields may be sufficient for domestic and stock use.

Pco

### CONNOQUENESSING FORMATION

Medium- to fine-grained gray sandstone containing lenses of dark-gray shale and discontinuous beds of Quakertown coal. Yields moderate quantities of water that is locally high in iron content.



### SHENANGO FORMATION

The upper member (Msu) is composed of soft medium-to dark-gray shale with interbeds of siltstone and lenses of fine-grained sandstone. Unimportant as an aquifer. The lower member (Msi) is composed of medium-to fine-grained light-gray sandstone and medium-to dark-gray shale and siltstone. Yields moderate to large quantities of water that is locally high in iron content at shallow depths.

Pp

### POTTSVILLE UNDIFFERENTIATED

Sandstones, possibly containing some relatively thick beds of shale; correlation with Connoquenessing, Mercer, and Homewood Formations uncertain. Unimportant as an aquifer.

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